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# **Transport Properties of Inhomogeneous Fluid Mixtures**<sup>1</sup>

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Explicit expressions for the transport coefficients of mixtures of dense, strongly inhomogeneous fluids are derived in terms of the equilibrium structure factors of such mixtures, in the framework of the nonequilibrium statistical mechanical theory suggested by the authors. Particular attention is paid to the diffusion coefficients of multicomponent inhomogeneous fluids. The case of binary diffusion in inhomogeneous fluids is considered in detail.

**KEY WORDS:** diffusion coefficients; fluids; inhomogeneous fluid mixtures; nonequilibrium statistical mechanics; transport coefficients; transport theory.

# **1. INTRODUCTION**

The thermodynamic properties of dense, strongly inhomogeneous fluids (both gases and liquids), such as those at interfaces or confined in narrow capillary pores of several molecular diameters in width, differ markedly from their counterparts for homogeneous (bulk) fluids. Such fluids and their mixtures (below called nanofluids or nanofluid mixtures) show new and modified phase transitions and transport properties, highly selective adsorption, spatially dependent structure properties, etc. Experimental investigation of thermodynamic properties of nanofluids and their mixtures is difficult, because of the complicated structure of the confined systems and

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interfaces, the many variables involved, and the sensitivity of the properties to experimental conditions.

Although over the last decade there has been significant development in understanding equilibrium properties of inhomogeneous fluids, much less progress has been made in the case of transport properties. Such knowledge is very important for both basic and applied research, since many industrial processes are known to be limited by diffusion, selectivity, and/or flow considerations.

Over the last few decades, several successful statistical mechanical approaches to microscopic theory of transport processes have been developed for homogeneous fluids (see, e.g., Refs. 1-6). However, there have been few attempts to develop a statistical mechanical theory of transport processes in nanofluids, in particular, in nanofluids of liquid-like density [7-9]. Recently the authors of this paper have suggested a rigorous, nonequilbrium statistical mechanical approach  $\lceil 10^{-14} \rceil$  to transport processes in nanofluids and their mixtures. This approach incorporates and develops basic mathematical techniques and ideas featured in nonequilibrium statistical mechanics of bulk fluids, including the representation of intermolecular interaction potentials as sums of hard-core repulsive and soft attractive contributions [6]. Also, the approach utilizes the authors' generalization of the Mori-Zwanzig projection operator method to establish kinetic and transport theories of nanofluids [10-13], and, recently, of nanofluid mixtures [14]. These theories tolerate any specific geometry of a confined system or interface (arbitrary pore shape, width, structure of pore walls; arbitrary form of an interface, etc.) and supply explicit expressions for transport coefficients of nanofluids and their mixtures. The derived transport coefficients are related to equilibrium structure properties (the densities, the pair and direct correlation functions) of the nanofluids or the nanofluid mixtures. The above theoretical results have been tested against nonequilibrium molecular dynamics (NEMD) simulation data for the shear viscosity of a simple nanofluid confined in narrow slit pores about 5 molecular diameters in width [13]. The theory correctly predicts an increase in the shear viscosity of up to 50% due to confinement and the oscillatory nature of the local shear viscosity. The agreement between the theoretical and the NEMD data is within 1 to 5 %.

# **2. TRANSPORT PROPERTIES OF NANOFLUID MIXTURES**

In this paper we report our latest results on the transport coefficients of nanofluid mixtures. For further analytical details and explicit expressions for the viscosities and thermal conductivities of nanofluid mixtures, we refer readers to our recent paper [14]. However, the diffusion coefficients of the

nanofluid mixtures are considered in greater detail below in view of their importance in applications.

In what follows we consider a mixture of *N* fluid components composed of simple, structureless molecules in a confinement of arbitrary shape. The walls are formed by simple, structureless molecules, all of the same species, immovable from their positions in the walls, and thermostated at temperature *T.* Inhomogeneity of the nanofluid mixture is caused by the continuous external potential field, represented as a sum of shortrange repulsive and long-range attractive contributions. The repulsive part describes hard-core-like interactions of the fluid molecules with the wall molecules forming the confinement. The attractive contributions are caused by both the long-range intermolecular interactions of the fluid molecules with the molecules of the walls and an external potential field of a general nature. A similar representation can be used for the fluid-fluid molecule interactions by means of the Weeks, Chandler, and Andersen (WCA) or Barker and Henderson (BH) methods. The repulsive contributions to all of the potentials of intermolecular interaction are assumed to be hard-core ones, with the effective diameters  $\sigma_{ij}$  specific to interactions of the *i*th species molecules with those of the *jth* species, and with the effective diameters  $\sigma_{iw}$  corresponding to the repulsive interactions of the *i*th species molecules with those of the walls. The attractive parts of the potentials behave as  $r^{-n}$ ,  $n > 2$ , at  $r \to \infty$ , where r is the distance between interacting molecules. The potentials of intermolecular interaction are central and pairwise. In addition, we assume that there is no chemical reaction in the system.

Under the above conditions, we can use Eq. (4.1) of Ref. 14 for the diffusion velocity of the *i*th component of the nanofluid mixture and the generating expression for the tensorial diffusion coefficients, Eq. (4.3), derived there. This expression represents the local values of the tensorial diffusion coefficients of the nanofluid mixture in terms of its local equilibrium pressure,  $P(q)$  at the point q. For the nanofluid mixture described above, the equilibrium pressure can be written in terms of the equilibrium structure factors of the nanofluid mixture,

$$
\mathbf{P}(\mathbf{q}) = \sum_{i=1}^{N} \sum_{j=1}^{N} \left\{ n_i(\mathbf{q}) k_{\mathbf{B}} T \left[ \delta_{ij} + \frac{1}{4\pi} b_{ij} n_j(\mathbf{q}) \int d\hat{\sigma} g_{ij}(\mathbf{q}, \mathbf{q} - \sigma_{ij} \hat{\sigma}) \right] - \frac{1}{6} n_i(\mathbf{q}) n_j(\mathbf{q}) \int_{\sigma_{ij} \hat{\sigma}}^{\infty} d\mathbf{r} g_{ij}(\mathbf{q}, \mathbf{q} + \mathbf{r}) \left[ \frac{\partial \phi_{ij}(\mathbf{r})}{\partial \mathbf{r}} \cdot \mathbf{r} \right] |\mathbf{r}|^2 \right\}
$$
(1)

where  $\phi_{ij}(\mathbf{r})$  is the attractive part of the intermolecular interaction potential for the *i*th and *j*th components;  $k_B$  is the Boltzmann constant;  $n_i(q)$ ,

 $i = 1,..., N$  are the equilibrium density profiles of the components;  $\delta_{ij}$  denotes Kronecker's delta;  $b_{ij} = \frac{2}{3}\pi \sigma_{ij}^3$ ;  $g_{ij}(\mathbf{q}, \mathbf{q} - \sigma_{ij}\hat{\sigma})$  and  $g_{ij}(\mathbf{q}, \mathbf{q}')$  are values of the pair correlation function calculated at different locations of the *i*-component and *j*-component molecules,  $\hat{\sigma} = \sigma_x \mathbf{i} + \sigma_y \mathbf{j} + \sigma_z \mathbf{k}$  is the unit vector  $(\sigma_x^2 + \sigma_y^2 + \sigma_z^2 = 1)$ ; **i**, **j**, **k** are unit vectors of the directions of the adopted Cartesian system of coordinates; integration over  $\hat{\sigma}$  is integration over the surface of the unit sphere, and the integral over r is a regular volume integral.

Using Eq. (1) one can derive from Eq. (4.3) of Ref. 14 the following expression for the Fourier image obtained by the time Fourier transform of the local tensorial mutual diffusion coefficient,  $\hat{\mathbf{D}}_{i\alpha}(\mathbf{q},\omega)$ ,

$$
\hat{\mathbf{D}}_{i\alpha}(\mathbf{q}, \omega) = \left\{ E_{i\alpha}(\mathbf{q}) + \sum_{k \neq i}^{N} \Omega_{ik}(\mathbf{q}, \omega) E_{k\alpha}(\mathbf{q}) \hat{\mathbf{\Omega}}_{ik}(\mathbf{q}) + \sum_{k \neq i}^{N} \sum_{l \neq k}^{N} \cdots \sum_{j \neq s}^{N} \Omega_{ik}(\mathbf{q}, \omega) \Omega_{ik}(\mathbf{q}, \omega) \cdots \Omega_{js}(\mathbf{q}, \omega) E_{js}(\mathbf{q}) + \times \hat{\mathbf{\Omega}}_{ik}(\mathbf{q}) \cdot \hat{\mathbf{\Omega}}_{ik}(\mathbf{q}) \cdots \cdot \hat{\mathbf{\Omega}}_{js}(\mathbf{q}) \right\} \mathbf{I}
$$
\n(2)

where  $\alpha = 1,..., N$ , and  $\omega$  is the frequency. In what follows  $m_i$  is the mass of a molecule of the /th fluid component of the mixture, the subscript *w* refers to the walls,  $\beta = 1/k_B T$ , the subscript *d* refers to diffusion, **I** is the unit matrix, and the rest of the notation is given below:

$$
\overline{\tau_{id}(\mathbf{q})} \equiv \frac{3\sqrt{\pi\beta m_i}}{2\sigma_{ii}^2} \tau_{id}(\mathbf{q})
$$
\n(3)

$$
\tau_{id}^{-1}(\mathbf{q}, \omega) \equiv \sum_{k \neq i}^{N} \frac{\sqrt{2m_k/m_i} \sigma_{ik}^2}{[1 + m_k/m_i]^{1/2} \sigma_{il}^2} \int d\hat{\sigma} \, n_k(\mathbf{q} - \sigma_{ik}\hat{\sigma}) \, g_{ik}(\mathbf{q}, \mathbf{q} - \sigma_{ik}\hat{\sigma})
$$

$$
- \frac{\sqrt{2} \, \sigma_{iw}^2}{\sigma_{il}^2} \int d\hat{\sigma} \, n_w(\mathbf{q} - \sigma_{iw}\hat{\sigma}) \, g_{iw}(\mathbf{q}, \mathbf{q} - \sigma_{iw}\hat{\sigma}) \tag{4}
$$

$$
\tau_{id}^*(\mathbf{q}, \omega) = \frac{\tau_{id}(\mathbf{q})}{\left[1 - i\omega \tau_{id}(\mathbf{q})\right]}
$$
(5)

$$
\Omega_{ik}(\mathbf{q},\omega) = \frac{3\sqrt{2}m_i\sigma_{ik}^2n_i(\mathbf{q})}{\left[1+m_k/m_i\right]^{1/2}\sigma_{kk}^2n_k(\mathbf{q})}\,\tau_{kd}^*(\mathbf{q},\omega) \tag{6}
$$

$$
\hat{\mathbf{\Omega}}_{ik}(\mathbf{q}) = \int d\hat{\sigma} \; n_k(\mathbf{q} - \sigma_{ik}\hat{\sigma}) \; g_{ik}(\mathbf{q}, \mathbf{q} - \sigma_{ik}\hat{\sigma}) \left[ \; \hat{\sigma}\hat{\sigma} - \frac{1}{3} \; \mathbf{I} \; \right] \tag{7}
$$

$$
E_{il}(\mathbf{q}) = \frac{1}{\beta} \left\{ \delta_{il} + \frac{1}{2\pi} n_i(\mathbf{q}) b_{il} \int d\hat{\sigma} g_{il}(\mathbf{q}, \mathbf{q} - \sigma_{il}\hat{\sigma}) \right.+ \frac{1}{4\pi} \sum_j n_i(\mathbf{q}) n_j(\mathbf{q}) \int d\hat{\sigma} \frac{\partial g_{ij}(\mathbf{q}, \mathbf{q} - \sigma_{ij}\hat{\sigma})}{\partial n_i(\mathbf{q})}- \frac{\beta}{3} n_i(\mathbf{q}) \int_{\sigma_{il}\hat{\sigma} + \mathbf{q}}^{\infty} d\mathbf{q}'' |\mathbf{q}''|^2 \mathbf{q}'' \cdot \frac{d\phi_{il}(\mathbf{q}'')}{d\mathbf{q}''} g_{il}(\mathbf{q}, \mathbf{q}'')- \frac{\beta}{6} \sum_j n_i(\mathbf{q}) n_j(\mathbf{q}) \int_{\sigma_{ij}\hat{\sigma} + \mathbf{q}}^{\infty} d\mathbf{q}'' |\mathbf{q}''|^2 \mathbf{q}'' \cdot \frac{d\phi_{ij}(\mathbf{q}'')}{d\mathbf{q}} \frac{\partial g_{ij}(\mathbf{q}, \mathbf{q}'')}{\partial n_i(\mathbf{q})} \right\}
$$
(8)

Expression  $(5)$  defines the diffusion relaxation time specific to the *i*th component.

The diffusion coefficients of Eq. (2) come into Eq. (4.3) of Ref. 14 with the gradients of the equilibrium densities of the components, which are not all linearly independent. The dependent component density can be excluded upon the use of Eq. (1). This leads to the final expression for the theoretical diffusion coefficients of the nanofluid mixture:

$$
\left[\hat{\mathbf{D}}_{il}(\mathbf{q},\omega)\right]_T = \frac{3\tau_{id}^*(\mathbf{q},\omega)\,\rho_l(\mathbf{q})}{2\sigma_{il}^2 n_i(\mathbf{q})\,\rho(\mathbf{q})}\sqrt{\frac{\pi\beta}{m_i}} \left[\,\hat{\mathbf{D}}_{il}(\mathbf{q},\omega) - \frac{P_l(\mathbf{q})}{P_m(\mathbf{q})}\,\hat{\mathbf{D}}_{im}(\mathbf{q},\omega)\,\right] \tag{9}
$$

where  $P_{\ell}(q) = \sum_{i=1}^{N} E_{\ell}(q)$ ,  $\rho(q) = \sum_{i=1}^{N} \rho_{i}(q)$ , and *m* is the index of the linearly dependent density. The diffusion coefficients of Eq. (9), in their turn, are not linearly independent, and satisfy the condition,

$$
\sum_{i} m_{i} n_{i}(\mathbf{q}) \left[\hat{\mathbf{D}}_{ii}(\mathbf{q}, \omega)\right]_{T} = 0 \tag{10}
$$

which follows from the restriction  $\sum_{i=1}^{N} m_i n_i(\mathbf{q}) \mathbf{V}_i(\mathbf{q},\omega) = 0$  on the diffusion velocities of the components,  $V_i(q, \omega)$ . At zero frequency,  $\omega = 0$ , from Eqs. (9) and (10) one can derive the local values of the frequency-independent diffusion coefficients of the nanofluid mixture.

### **2.1. Phenomenological Diffusion Coefficients of Nanofluid Mixtures**

The local values of the phenomenological diffusion coefficients  $\hat{\mathbf{D}}_{u}^{p}(\mathbf{q})$  are defined by the expression for the mass flux of the *i*th component,  $J_i^p(q)$ ,

$$
\mathbf{J}_i^p(\mathbf{q}) = m_i n_i(\mathbf{q}) \mathbf{V}_i(\mathbf{q})
$$
  
= 
$$
- \sum_{l \neq m} \hat{\mathbf{D}}_{il}^p(\mathbf{q}) m_l \cdot \frac{\partial n_l(\mathbf{q})}{\partial \mathbf{q}} - \hat{\mathbf{D}}_i^T(\mathbf{q}) \left( \frac{\partial \ln T(\mathbf{q})}{\partial \mathbf{q}} \right)
$$
(11)

where  $\hat{\mathbf{D}}_i^T(\mathbf{q})$  is the thermal diffusion coefficient, and the dot  $\cdot$  denotes the inner product. On the other hand, the theoretical diffusion coefficients are proportionality coefficients between the diffusion velocities and the gradients of the densities of the components,

$$
\mathbf{V}_i(\mathbf{q}, \omega) = -\sum_{l \neq m} \left[ \hat{\mathbf{D}}_{il}(\mathbf{q}, \omega) \right]_T \frac{\partial n_l(\mathbf{q})}{\partial \mathbf{q}}
$$

Substitution of Eq. (9) calculated at  $\omega = 0$  into Eq. (11) leads to the relation,

$$
\hat{\mathbf{D}}_{il}^{p}(\mathbf{q}) = \frac{m_{i}}{m_{l}} n_{i}(\mathbf{q}) \left[ \hat{\mathbf{D}}_{il}(\mathbf{q}) \right]_{T}
$$
\n(12)

between local values of the theoretical and phenomenological diffusion coefficients.

## 2.2. **Binary Diffusion in Nanofluid Mixtures**

In the case of weak inhomogeneity of the nanofluid mixture, the terms with sums on the right hand side of Eq. (2) can be neglected, and from Eqs.  $(2)$ ,  $(4)$ ,  $(5)$ ,  $(9)$ , and  $(10)$  it follows that the theoretical diffusion coefficient of the binary mixture,  $[\hat{\mathbf{D}}_{12} (\mathbf{q})]_T$ , at  $\omega = 0$  is

$$
\begin{aligned}\n\left[\hat{\mathbf{D}}_{12}(\mathbf{q})\right]_T &= \frac{4D_{12}^*(\mathbf{q})\,n(\mathbf{q})\,\beta m_2 n_2(\mathbf{q})}{n_1(\mathbf{q})\int d\hat{\sigma} \,n_2(\mathbf{q} - \sigma_{12}\hat{\sigma})\,g_{12}(\mathbf{q}, \mathbf{q} - \sigma_{12}\hat{\sigma})\,\rho(\mathbf{q})} \\
&\times \left[E_{12}(\mathbf{q}) - \frac{P_2(\mathbf{q})}{P_1(\mathbf{q})}\,E_{11}(\mathbf{q})\right]\mathbf{I}\n\end{aligned} \tag{13}
$$

where

$$
D_{12}^*(\mathbf{q}) = \frac{3\sqrt{2\pi k_\mathrm{B}T}}{16\pi\sigma_{12}^2 n(\mathbf{q})\sqrt{m_{12}}} \quad \text{and} \quad m_{12} = \frac{m_1 m_2}{m_1 + m_2}
$$

 $E_{il}(\mathbf{q})$  is given by Eq. (8), and  $P_l(\mathbf{q})$  is defined by Eq. (9).

From Eqs. (13) and (12) one can derive the following relation between the two phenomenological diffusion coefficients of a weakly inhomogeneous binary mixture of nanofluids,

$$
\widehat{\mathbf{D}}_{12}^P(\mathbf{q}) = \left[ \frac{m_1 P_2(\mathbf{q})}{m_2 P_1(\mathbf{q})} \right] \left[ \frac{n_2(\mathbf{q}) \int d\hat{\sigma} n_1(\mathbf{q} - \sigma_{12}\hat{\sigma}) g_{12}(\mathbf{q}, \mathbf{q} - \sigma_{12}\hat{\sigma})}{n_1(\mathbf{q}) \int d\hat{\sigma} n_2(\mathbf{q} - \sigma_{12}\hat{\sigma}) g_{12}(\mathbf{q}, \mathbf{q} - \sigma_{12}\hat{\sigma})} \right] \widehat{\mathbf{D}}_{21}^P(\mathbf{q})
$$
\n(14)

In the particular case of a binary mixture of bulk fluids, this expression reduces to

$$
\widehat{\mathbf{D}}_{12}^p = \left[ \frac{m_1 P_2}{m_2 P_1} \right] \widehat{\mathbf{D}}_{21}^p
$$

where  $\hat{\mathbf{D}}_{12}^p$  is the homogeneous reduction of the corresponding phenomenological coefficient, Eq. (12), expressed in terms of the theoretical diffusion coefficient, Eq. (13), calculated for the homogeneous mixture. This relation has been derived rigorously in the framework of a microscopic approach in Ref. 17 for a binary mixture of hard spheres in the framework of the Chapman-Enskog method. Here we have generalized this result and proved that the same relation also holds for a binary mixture of arbitrary bulk fluids, provided that their intermolecular interaction potentials can be divided into a sum of hard-core repulsive and soft attractive contributions.

From the results of Ref. 14 it follows that the diffusion coefficients of the nanofluid mixture depend strongly on the equilibrium pressure of the mixture, which in the above case depends explicitly on the attractive part of the intermolecular interaction potentials [see Eq.  $(1)$ ]. This also means that the values of the diffusion coefficients are very sensitive to a particular approximation of the equilibrium pressure of the nanofluid mixture. In this respect, the diffusion coefficients differ significantly from the viscosities and thermal conductivity coefficients of such mixtures, Eqs.  $(3.24)$ – $(3.26)$ and (3.32) of Ref. 14, which do not depend on the equilibrium pressure explicitly.

## **3. CONCLUSIONS**

Calculation of the transport coefficients based on Eqs. (3.24)-(3.26) and  $(3.32)$  of Ref. 14 and the above equations [Eqs. (13), (9), and (2)] require data on equilibrium structure factors of the nanofluid mixtures, in particular, on the number densities of the components  $n_i(q)$  and the contact values of their pair correlation functions,  $g_{il}(\mathbf{q}, \mathbf{q} - \sigma_{il}\hat{\sigma})$ . These coefficients also depend on the effective hard-core diameters,  $\sigma_{il}$ , evaluated for the intermolecular interaction potentials, which are divided into a sum of hard-core repulsive and soft attractive contributions. Such intermolecular interaction potentials can be obtained from more realistic intermolecular interaction potentials (e.g., the Lennard-Jones model potentials) by means of Weeks, Chandler, and Andersen (WCA) [15] or Barker and Henderson (BH) [16] methods. The WCA method supplies hard-core diameters  $\sigma_{il}^{WCA}$  which depend on both the temperature and the equilibrium number densities of the components of the mixture, whereas the

BH procedure leads to  $\sigma_{il}^{BH}$ 's that depend only on temperature. From a dynamical point of view the differences between collisional encounters described by the model potentials of this theory and more realistic ones are small.

In order to avoid calculation of  $\sigma_{il}$ 's for every local set of values of  $n_i(q)$ ,  $i = 1,..., N$ , one can use the BH choice of hard-core diameters, which do not depend on the densities of the components or the density of the mixture. In the case of the nanofluid mixtures confined in narrow capillary pores, this seems to be the best choice for the hard-core diameters [6].

The structure properties of the nanofluid mixtures can be obtained by direct equilibrium computer simulations. These results can be expressed in dimensionless form and, as such, are valid for any  $\sigma_{il}$  and  $n_i(q)$ . Another possibility is to determine the structure by analytical means from integral equations of equilibrium statistical mechanics and/or in the framework of density functional theory. For practical purposes direct computer simulation data seem to be more useful, as they should reflect the structure of a particular nanofluid system in greater detail.

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